

Version 19.0

Build	Module	Description	ID
10.09.19	Analyses	The partial safety factors for the earth pressure at rest and increased active earth pressure in the base failure, respectively, sliding analysis have been corrected.	13745
26.04.19	Design	The maximum admissible steel strain is limited for thin slab-like structural members with double layer reinforcement, since the compressive zone would be too small otherwise. The limitation is required, since otherwise there is the possibility, that the tensile zone covers both reinforcement layers at the top and at the bottom. As a result, the compressive zone would only be in the area of the concrete coverage. This prevents the increase of both reinforcement layers during the design, which would lead to inefficient results.	13255
26.04.19	Output document	The ground level was not dimensioned in the result graph.	13074
26.04.19	Analyses	Sometimes the load components were not correctly considered with regard to favorable or unfavorable effects in the calculation of the soil stresses.	13110
26.04.19	Calculation	By default, the foundation settlement at the left outer edge (Point A) and the right outer edge (Point B) is being issued. When there is a gaping joint, Point B shifts from the right outer edge into the inside of the foundation up to the point of zero stress. Settlement and position of the new point B are issued for a gaping joint.	13163
26.04.19	Design	<p>The following approach in the design is valid for the application of the compaction earth pressure under consideration of the user specifications:</p> <ol style="list-style-type: none"> Filling width B is specified In this case, the earth pressure stress ev_h for the rigid wall is calculated by the program: <ul style="list-style-type: none"> for $B \leq 1,0m$ is $ev_h = 40 \text{ kN/m}^2$ for $B \geq 2,50m$ is $ev_h = 25 \text{ kN/m}^2$ interim values for B are linearly interpolated z_p is calculated according to formula 64 in dependency of the calculated earth pressure stress Earth pressure stress ev_h is specified In this case, the specification of the earth pressure stress is used <ul style="list-style-type: none"> only the application depth z_p will be calculated by the program with formula 64 always the specified stress is applied independently from the earth pressure approach <p>Independently of this approach, the following applies for the three cases active earth pressure, earth pressure at rest and increased active earth pressure: For the <u>active earth pressure</u>, the compaction earth pressure ends at $z_a = 2,0m$. For the <u>earth pressure at rest</u> does z_a not exist. The compaction earth pressure is intersected with the earth pressure at rest curve and ends at the intersection point. For the <u>increased active earth pressure</u>, the end of the compacting earth pressure is intersected between z_a for the active earth pressure and the earth pressure at rest. There is a constant ev_h in both cases, however.</p>	12845
26.04.19	Output document	The settlements are now output for the points A (left foundation edge) and B' (intersection of the stress curve with the bottom edge of the foundation with a gaping joint) with an existing gaping joint in the foundation slab.	13249
26.04.19	User interface	Was the load value of a load onto the wall marked, then an input window with the wrong unit [m] opened.	12681

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Build	Module	Description	ID
16.05.18	Design	When generating the interface file for the design with NaZwei it could happen, that the file path was read-only (installation directory) and that this caused the termination of the design.	12606
01.03.18	Analyses	For ground water levels above the foundation level, the overlying soil layers are now applied with the weighted averages of the dry and the buoyant unit weight.	12370
01.03.18	Analyses	The geotechnical analyses as well as the design can now be carried out with or without compaction earth pressure independent of each other. The size of the compaction earth pressure always depends on the relevant earth pressure approach of the corresponding analysis. It is hereby distinguished between the compaction earth pressures for active earth pressure or earth pressure at rest. For an increased active earth pressure approach, it is being interpolated between the compaction earth pressure for active earth pressure and for the earth pressure at rest.	12361
01.03.18	Analyses	The application of the compaction earth pressure as decisive loading is now also possible for the geotechnical analyses.	9218
01.03.18	Calculation	Up to 1000 circles can now simultaneously be calculated in the slip circle analysis.	11736
01.03.18	Design	The options for the analysis in the SLS could not separately be specified for multiple system variants.	9990
01.03.18	Design	In the design of the wall, the compaction earth pressure is now also considered correctly for an increased active earth pressure.	8163
01.03.18	Input	There is now a warning message displayed, if the ground inclination is greater than phi.	11630
01.03.18	Input	There is now a warning, if a ground run with varying inclinations exists although the earth pressure option "Wall friction angle = ground inclination" has been set.	11629
01.03.18	Output document	The section "Settlement analysis in the SLS" has been extended with a legend.	11784
01.03.18	Output document	The calculated values for z_p and z_a of the compaction earth pressure are now also issued.	8186
01.03.18	User interface	There is now a warning message, if a single load or single moment is automatically removed by modifying the wall cross-section.	9997
01.03.18	Analyses	The partial safety factors for the design situations BS-T and BS-A are now provided in the options for the analysis of the safety against displacement in the limit state EQU.	11783
01.03.18	Analyses	The partial safety factors for the design situations BS-T and BS-A are now provided in the options for the analysis of the safety against displacement in the limit state EQU.	11143
01.03.18	Calculation	A stabilizing load was possibly not considered anymore in the base failure analysis.	11898
01.03.18	Calculation	A mistake in the calculation of loading onto a soil body, if the ground level is $>\phi$ and an dragging section, has been fixed.	11626
01.03.18	Design	With a combination of the design options "Design with an increased active earth pressure" and design with "Compaction earth pressure" the program terminated during the design.	11400
01.03.18	Input	The increment has been corrected from 5.0 to 1.0 in the dialog "Generate user-defined earth pressure". Furthermore, the last entered value is now saved when leaving the dialog via "OK".	10912
01.03.18	Output document	The geometry of the slope was not issued.	11792
01.03.18	Output document	The headings of the required reinforcement amounts were incorrect in the overview of the analyses. The adding " (LF BS-P(1g)) " was issued for the required longitudinal and shear reinforcement in the ULS and SLS.	10234
01.03.18	Output document	The text of the design situation was cut off in the tables of single loads and moments onto the wall in the record of the input.	9992
01.03.18	Output document	The relevant design situation is now stated in the caption of the base failure shell graph.	9987

Release Notes

LIMES



Build	Module	Description	ID
01.03.18	Output document	The decisive rotation point at the bottom left corner in the analysis of the structural equilibrium was not correctly issued, if the z-direction is upward.	9420
01.03.18	User interface	The editing of polygonal elements is now made via the external application RTpoly.	11309
01.03.18	User interface	The display of the soil layer boundaries of a shifted coordinate system is now limited to the wall segment.	9978

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Build	Module	Description	ID
13.04.17	Design	The calculation of the loading onto a bracket existing groundwater was incorrect. Too much weight has been applied in the consideration of the soil dead load above a bracket for inclined walls.	11246
06.04.17	General	The slip circle module has been optimized, so that the calculation time for the individual analysis could be reduced significantly. In the process, a license query had been included by mistake, which enabled leading the slip circle analysis in the program without an existing Gleitk license.	11212
10.03.17	General	Program maintenance and support	11095
10.03.17	Calculation	The load was not correctly calculated in the calculation of earth surcharge loads onto a bracket, if the rear edge of the wall above the bracket did not run vertically.	11061
10.03.17	Calculation	The earth resistance of the horizontal substitute shear joint was applied too low in the sliding analysis. A wrong partial safety factor was used for an increased active earth pressure.	9894
10.03.17	Design	A wrong partial safety factor was used in the design of the wall with the selected option "Earth pressure at rest" for a calculation with an increased active earth pressure.	9989
10.03.17	Design	Single loads onto the wall were incorrectly considered in the calculation of internal forces at a design section in the keel on the downstream side.	9431
10.03.17	Output document	The overturning analysis is initially carried out for the 1. core width (only permanent loads) and then again for the 2. core width (permanent + variable loads). Misleadingly, the two analyses had different headings. Now, the two analyses are also listed right below each other.	9653
10.03.17	Output document	The characteristic earth pressure stresses had, both for the earth pressure from permanent loads and for the total earth pressure from g and q, the same headings.	9223