

### Version 18.0

Build	Module	Description	ID
16.05.18	Design	When generating the interface file for the design with NaZwei it could happen, that the file path was read-only (installation directory) and that this caused the termination of the design.	12607
01.03.18	Analyses	For ground water levels above the foundation level, the overlying soil layers are now applied with the weighted averages of the dry and the buoyant unit weight.	12373
16.02.18	Analyses	For a "pressure balance" of the horizontal forces there is now the new option "calculated mobilized earth resistance". The earth resistance is hereby reduced thus far, that it does not exceed the back pressure of the active side.	9806
16.02.18	Calculation	Up to 1000 circles can now simultaneously be calculated in the slip circle analysis.	11738
16.02.18	Design	The stress resultants and the calculated reinforcement of non-permanent load cases (e.g. BS-T) were equal to the permanent load cases.	7234
16.02.18	Output document	The section "Settlement analysis in the SLS" has been extended with a legend.	10864
16.02.18	Analyses	The partial safety factors for the design situations BS-T and BS-A are now provided in the options for the analysis of the safety against displacement in the limit state EQU.	11781
16.02.18	Calculation	A stabilizing load was possibly not considered anymore in the base failure analysis.	11899
16.02.18	Calculation	There was an error in the calculation of the resultant in the base joint for load case 1g.	11730
16.02.18	Input	The increment has been corrected from 5.0 to 1.0 in the dialog "Generate user-defined earth pressure". Furthermore, the last entered value is now saved when leaving the dialog via "OK".	11787
16.02.18	Output document	The name of the load case is no longer cut-off in the table of the single loads onto the wall.	8226
16.02.18	User interface	The editing of polygonal elements is now made via the external application RTpoly.	11780

### Version 17.0

Build	Module	Description	ID
06.04.17	General	The slip circle module has been optimized, so that the calculation time for the individual analysis could be reduced significantly. In the process, a license query had been included by mistake, which enabled leading the slip circle analysis in the program without an existing Gleitk license.	11214
02.03.17	Design	A wrong partial safety factor was used in the design of the wall with the selected option "Earth pressure at rest" for a calculation with an increased active earth pressure.	11079
02.03.17	Output document	The characteristic earth pressure stresses had, both for the earth pressure from permanent loads and for the total earth pressure from g and q, the same headings.	11081
02.03.17	Output document	The overturning analysis is initially carried out for the 1. core width (only permanent loads) and then again for the 2. core width (permanent + variable loads). Misleadingly, the two analyses had different headings. Now, the two analyses are also listed right below each other.	11080
02.03.17	Output document	The "Analysis of the static equilibrium" appeared in the summary of the earth static analysis, although it is not carried out in PINwalls.	9969
02.03.17	Output document	The type of loading (permanent or live load) was not completely issued in the record of the input of the wall loads.	9904

### Version 16.0

Build	Module	Description	ID
08.03.16	Calculation	In the calculation of the base pressure according to DIN 1054:2010 always a $\sigma_{exis} = 0$ was issued, so that the analysis was always fulfilled.	9651
05.02.16	Calculation	Revision and improvement of the numerical earth pressure calculation with the KEM-method according to CULMANN. The calculation of the earth resistance with the KEM-method (Gudehus) is no longer necessary and has been removed to improve the performance of the program.	9629
05.02.16	General	Program modifications for the <b>compatibility with Windows 10</b> .	9525

### Version 15.0

Build	Module	Description	ID
02.06.15	User interface	In the consideration of the cohesion according to DIN 4085 the increase of $\min K_{ah}$ for a slope is now possible.	9101
02.06.15	User interface	The program termination when opening the dialog "Earth pressure options" due to the missing option "Increase of $\min K_{ah}$ for a slope" has been fixed.	9086
16.04.15	User interface	$h_u$ and $h_o$ were labeled as concrete cover in the input as well as in the output, although they are considered as reinforcement layer (reinforcement centre distance).	8944
27.02.15	Analyses	The <b>analysis of the terminated cracking under CSN EN</b> standards is performed on the basis of the general EN 1992-1-1 again, whereupon the coefficient $k_3$ for the calculation of the crack spacing $s_{r,max}$ is calculated according to a change (2015) in the national annex of the CSN EN.	8820
05.02.15	Calculation	The transfer of the soil engineering standard to the slip circle analysis malfunctioned. The slip circle was always calculated according to DIN 1054:2005 independently from the standard settings in the program.	8143
05.02.15	Output document	Only the results of the currently selected model were issued in the result overview for multiple system models, even if all models had been calculated.	8705

### Version 14.0

Build	Module	Description	ID
24.06.14	Input	The input of the extent of the ground on the left via the visibilities failed for several system variants. Now it can be additionally modified via a dimension chain.	7893
24.06.14	Calculation	The earth pressure due to the slope was miscalculated for an embankment.	7571
23.01.14	Analyses	<b>Sliding analysis</b> For an inclined foundation joint according to EN standards, the $T_d$ was not converted to the inclination.	7300
23.01.14	Calculation	For block loads, which are on an inclined ground surface, always 100% earth pressure at rest was applied for increased active earth pressure.	7509
23.01.14	Calculation	If the option "Consider earth pressure via soil dead load" was activated and the option "Earth pressure calculation according to Culman" was deactivated, the soil dead load was still considered.	7502
23.01.14	Calculation	Earth pressure at rest coefficient according to DIN 4085-100 was incorrect, if the wall friction angle $\delta$ was greater than the surface inclination $\beta$ .	7224
23.01.14	Calculation	Vertical, negative slopes have no longer been considered for earth pressure and earth resistance.	7217
23.01.14	Design	The material parameters of the DIN were always used, if a standard other than DIN 1045-1:2008 had been selected. This caused, that - for instance - the wrong values were used for a user-defined material whose parameters had been changed for EN.	7528
23.01.14	General	The program icon has been exchanged.	7220

Build	Module	Description	ID
23.01.14	Input	<b>Edit soil layer database</b> The data for delta, cohap and Es were not saved or were set to zero.	7514
23.01.14	User interface	The recent file list malfunctioned.	7506

### Version 13.0

Build	Module	Description	ID
24.06.13	Calculation	For an inclined rear edge of a masonry wall, the earth pressure has been calculated as if the wall was straight.	6821
24.06.13	Calculation	Earth pressure and earth resistance for vertical slopes and steep slopes malfunctioned.	6811
10.04.13	Calculation	The shape coefficient a (foundation length) for the base failure analysis can now be set. So far, this option was hardwired to the strip foundation.	6565
10.04.13	General	Now, the <b>release notes</b> are available in <b>English</b> .	6445
10.04.13	General	Program modifications for the <b>compatibility with Windows 8</b> .	6356
10.04.13	Output document	In the graphic "base failure shell" in the result list the left ground level is displayed.	6570
10.04.13	Design	The program no longer terminates when designing with user-defined concrete.	5331
10.04.13	General	Problems with the data path (a path length > appr. 130 characters led to an abnormal termination when opening the result list).	6172