Release Notes
PONTI®compositeConcrete

Version 18.0

Build	Module	Description	ID
09.08.18	General	Adjustments to the current program version TRIMAS® 18.0.	12859
12.06.18	General	Adjustments to the current program version TRIMAS® 18.0.	12688
07.05.18	General	Adjustments to the current program version TRIMAS® 18.0.	12556

Version 17.0

Build	Module	Description	ID
01.02.18	General	Adjustments to the current program version TRIMAS® 17.0.	12319
17.11.17	General	Adjustments to the current program version TRIMAS® 17.0.	12126
19.10.17	Interface	The analysis sections of the design now contain the corresponding element number from the TRIMAS calculation.	11635
05.05.17	General	Adjustments to the current program version TRIMAS® 17.0.	11358
02.05.17	General	Adjustments to the current program version TRIMAS® 17.0.	11339
14.03.17	Input	For unsymmetrical girders, the horizontal position of the centroid (ys) is informatively issued in the list.	10398
14.03.17	General	Adjustments to the current program version TRIMAS® 17.0.	11123

Version 16.0

Build	Module	Description	ID
28.11.16	Design	If there is solely being prestressed from the tendon end and the prestressing force is entered in kN instead of percent, then the input was still transferred as percent value. This caused, that the statically determined stress resultants were calculated from the maximum admissible prestressing force in the design. The total stress resultants from the static calculation remain unaffected.	10387
28.11.16	Input	The previous values were still issued in the protocol, after modifying the concrete quality in the cross-section input.	10400
14.10.16	General	The program terminated when starting the design or the secondary effects calculation, if the version of the result database (32 / 64-bit) did not correspond with the programs database. Now, a dialog with the appropriate message is displayed and the program is stopped.	9998
14.10.16	Design	**Decompression analysis** The initial prestressing steel stress Sig.p0 was wrongly applied without consideration of the concrete shortening in the creep and shrinkage calculation. The initial prestressing steel stress was corrected and thus the cross-section stresses are correct. For the time-depending stresses, however, the calculation was correct.	10213
14.10.16	Input	The nominal diameter dNom of a stressing bed prestressing is now also passed to the calculation.	10002
17.05.16	General	Adjustments to the current program version TRIMAS® 16.0.	9888
04.04.16	Design	The current psi2-value is issued for the quasi-permanent combinations in the list of the decompression in dependency of the prestressing type and the statical determination.	9681
16.02.16	General	Program modifications for the **compatibility with Windows 10**.	9529
16.02.16	General	Adjustments to the current program version TRIMAS® 16.0.	9671

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Version 15.0

Build	Module	Description	ID
15.12.15	General	The correct name of the requirement is now issued in the printout of the cross-section values for DIN EN.	9332
05.11.15	Design	If the possible support settlement is missing, then the probable support settlement without reduction is used in the basic combination.	9290
05.11.15	Design	Area live loads and axle loads are mutually exclusive in the superposition for pedestrian bridges now. The design is carried out for the more unfavorable value.	9230
15.09.15	General	Adjustments to the current program version TRIMAS® 15.0.	9315
02.08.15	General	Adjustments to the current program version TRIMAS® 15.0.	9204
20.05.15	Design	The dimensions of the diagram of the shear joint design were adjusted to the selected standard.	8976
22.04.15	Generation	The secondary construction states are generated automatically when entering a new project. Here, in the hitherto existing Version 15.0, the data from the previous construction state was only copied incompletely, so that the calculation of these new construction states was not possible.	8909
16.03.15	General	Adjustments to the current program version TRIMAS® 15.0.	8868
27.02.15	General	Adjustments to the current program version TRIMAS® 15.0.	8828
27.02.15	Design	In the ULS only the possible support settlements and in the SLS and FLS only the support settlements entered as probable are being considered.	8753
27.02.15	NAZWEI	**Hydration analysis of the in-situ concrete slab** The restraint force due to hydration is absorbed by the upper and lower reinforcement layer in the in-situ concrete slab. Only the upper layer is printed out though, since the program is only familiar with the following three reinforcement layers: In situ concrete slab, top / Precast component, top / Precast component, bottom. The same reinforcement due to hydration as in the upper layer has to be inserted in the "In-situ slab, bottom".	8723

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Version 14.0

Build	Module	Description	ID
02.02.15	Design	The decompression analysis at the time t=oo was not printed for restraint free systems (no secondary stress resultants).	8660
22.10.14	General	Adjustments to the current program version TRIMAS® 14.0.	8476
22.09.14	Design	For long beams with tendons ending in the beam length and with a very small spacing of the analysis sections, slightly unsymmetrical prestressing forces could appear in the output list due to differences in the position of calculation points of the prestressing and of the analysis sections. The calculation points of the prestressing are now adjusted to the analysis sections with an additional improved partition.	7807
22.09.14	Generation	Similar input parameter for the standard, partial safety coefficients and combination coefficients are now synchronized after changes between design program and calculation program.	8050
10.03.14	General	Adjustments to the current program version TRIMAS® 14.0.	7782
10.03.14	Design	**Analysis of the decompression under consideration of the secondary effects** A calculation of the secondary effects is necessary in statically indeterminate systems. Since these are determined at time too, but in the output the highest tensile stress from "before" and "after" too are issued, the positive effect of the secondary stress resultants in the column area was not considered. Furthermore, an error in the cross-section by cross-section stress output was corrected.	7786
10.03.14	Design	**Shear force design** The shear force design is now always performed with the inner lever arm from the bending design.	7756
10.03.14	Design	**Prestressing material** User-defined prestressing material is now added to the material list and considered correctly in the design.	7755
22.02.14	General	Adjustments to the current program version TRIMAS® 14.0.	7751
28.01.14	General	Adjustments to the current program version TRIMAS® 14.0.	7567
28.01.14	General	Adjustments to the current program version TRIMAS® 14.0.	7568

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Version 13.0

Build	Module	Description	ID
05.11.13	Design	**Minimum reinforcement due to the discharge of the hydration heat** The analysis is now limited to areas in which contacts between the in-situ concrete slab and the precast cross-section exist.	7257
10.10.13	Design	A composite cross-section cannot be designed if the in-situ concrete slab is smaller than the top flange of the precast element. An error message appears for such cross-sections.	7183
10.10.13	Design	In the shear design of composite joints in bridges the adhesion coefficients c are generally halved due to dynamic loading. For DIN EN 1992-2/NA and DIN 1045-1:2008 the c-values are set to 0.0.	7176
10.10.13	Design	**Design cross-section** The top flange of the design cross-section of composite I cross-sections has been generated incorrectly.	7109
04.09.13	Design	Adjustments in the graphical user interface and in the list output were made for the design according to DIN EN 1992-2/NA.	7037
04.09.13	Design	Cross-sections without prestressing and within the application area are now being ignored in the decompression analysis. Exceedings of the admissible stresses are only shown for the cross-section edge which is closer to the tendon.	7033
04.09.13	Design	**Short reinforcement edges in the top, respectively, bottom flange** Short reinforcement edges can arise e.g. by pushing together the bottom flange area, if a T-section is to be generated from a I-section. The reinforcement in these edges is ignored from now on.	7032
04.09.13	Input	In the dialog of the prestressing methods the selection after a reload is now also made with the material of the current tendon.	7039
08.07.13	Design	The bending design was incorrect for a reinforcement strain of 25 ‰.	6820
25.06.13	Design	**Minimum reinforcement due to run-off of the hydration heat in the in-situ concrete slab** The constraint forces from the runoff of the hydration heat are calculated and stated at composite cross-sections. It is assumed, that the tensile forces are only absorbed by the upper chord reinforcement in the in-situ concrete slab.	6695
25.06.13	General	Now, the **release notes** are available in **English**.	6459
25.06.13	General	Program modifications for the **compatibility with Windows 8**.	6372
25.06.13	General	The call up for the system modelling user guide has been added to the menu.	6159
25.06.13	Output document	**Support list with information about the support forces and deformations** According to DIN EN 1990/NA/A1:2012, a support list with corresponding support forces can be issued.	6818